

# Frequency domain identification of FIR models from noisy input–output data

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**Abstract:** This paper describes a new approach for identifying FIR models from a finite number of measurements, in the presence of additive and uncorrelated white noise. In particular, two different frequency domain algorithms are proposed. The first algorithm is based on some theoretical results concerning the dynamic Frisch scheme. The second algorithm maps the FIR identification problem into a quadratic eigenvalue problem. Both methods resemble in many aspects some other identification algorithms, originally developed in the time domain. The features of the proposed methods are compared with each other and with those of some time domain algorithms by means of Monte Carlo simulations.

Keywords: System identification; FIR models; Frisch scheme; Discrete Fourier Transform.

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## 1. INTRODUCTION

The estimation of finite impulse response (FIR) models from noise–corrupted data is an important problem in many signal processing applications [11; 20]. Most of the solutions proposed in the literature assume that only the output measurements are affected by noise. However, as observed in [3], in many practical situations the presence of an additive noise on the input is important as well and must be taken into account.

It is a well known result that the least–squares (LS) method gives biased parameter estimates when the input is affected by noise. On the contrary, a consistent estimate can be obtained by using the total least–squares (TLS) approach [3]. In this case, however, an additional assumption must be satisfied, since the ratio between the input and output noise variances must be *a priori* known.

There are several methods in the literature for how to get consistent parameter estimates for noise–corrupted FIR models. One options is to use the instrumental variables (IV) approach, [24]. Such IV algorithms are computationally efficient, but suffer of poor estimation precision [24].

In order to remove the bias of the LS estimates, many bias–compensated techniques have been proposed with several, different strategies, see e.g [5; 6] and the reference therein. The compensated least–squares (CLS) methods are quite attractive, since the particular structure of the FIR models allows to develop iterative least–squares algorithms that are particularly suited for on–line implementations, see e.g. [7] and the reference therein.

In this work the identification of FIR systems corrupted by additive white noise is addressed by using a frequency domain approach. In particular, two different frequency domain algorithms are proposed and their features are compared with each other and with some time domain methods.

From a theoretical point of view, there is a full equivalence between time and frequency domain identification methods, as shown for example in [1]. From the practical point of view, the decision to implement a time or a frequency domain algorithm can strongly depend on the user choices and on the specific applications. In most experimental situations the observations are collected as samples of time signals, so that a Fourier transformation is required before implementing a frequency domain algorithm. However, there also exist occasions in which the data are more easily available as frequency samples since they are collected by a frequency analyzer which directly provides the Fourier transforms of the time signals [14; 18].

The approach to be described in this paper for frequency domain identification of noisy FIR models has some similarities with related errors–invariables (EIV) problems [32; 33], where though the underlying structure is different. A common theme is that the estimation problem is formulated in the frequency domain in a way that takes all transient effects into account, as originally pointed out in [19]. As many other EIV approaches, also the proposed methods make use of the extended normal equations and require that some further equations are introduced, in order to get unique and consistent parameter estimates [24]. This being said about the similarities of the current paper and [32; 33], it is also crucial to note that the way the optimization criterions are introduced and analyzed is very highly tied to the specific model formulation (model parameterization), and therefore there are also large differences in the contents.

The organization of the paper is as follows. Section 2 defines the FIR plus noise identification problem in the frequency domain, while Section 3 introduces a novel frequency domain description of the FIR processes. Section 4 discusses some contexts for the identification of EIV models. In particular, the GIVE framework, originally proposed in [23] and the dynamic Frisch scheme, originally proposed in [2]. Sections 5 describes a possible identification criterion, that can be directly formulated in the frequency domain. In particular, this criterion takes advantage

of a set of equations similar to the High Order Yule Walker (HOYW) equations. The method can be considered as the application to FIR models of the frequency domain approach proposed in [31]. In Section 6, it is shown that as an alternative approach, the FIR identification problem can be reformulated as a quadratic eigenvalue problem involving only the output noise variance. The obtained quadratic eigenvalue problem is solved by mapping it into a generalized eigenvalue problem. The method can be considered as the frequency counterpart of the time domain approach proposed in [5]. In Section 7 some general issues of the FIR identification problem are discussed. In particular, the section treats the problem of estimating the correct order of the model and analyzes some practical aspects concerning the filtering operations in the frequency domain. In Section 8 the performance of the two proposed methods is tested by means of Monte Carlo simulations. Finally some concluding remarks are reported in Section 9.

## 2. STATEMENT OF THE PROBLEM

Consider the following FIR system, described by the difference equation

$$d(t) = H(z^{-1})x(t) \quad (1)$$

where  $x(t)$  and  $d(t)$  denote the input and output, and  $H(z^{-1})$  is the following polynomial in the backward shift operator  $z^{-1}$

$$H(z^{-1}) = h_0 + h_1 z^{-1} + \dots + h_{M-1} z^{1-M}. \quad (2)$$

The observations of  $x(t)$  and  $d(t)$  are both affected by additive noise, so that the available signals are

$$u(t) = x(t) + n_i(t) \quad (3)$$

$$y(t) = d(t) + n_o(t). \quad (4)$$

The following assumptions are made.

- A1. The length  $M$  of the FIR model is assumed as *a priori* known and  $h_{M-1} \neq 0$ .
- A2. The true input  $x(t)$  can be either a zero-mean ergodic process or a quasi-stationary bounded deterministic signal, i.e. such that the limit

$$\lim_{N \rightarrow \infty} \frac{1}{N} \sum_{t=1}^N x(t)x(t-\tau) \quad (5)$$

exists  $\forall \tau$  [14]. Moreover,  $x(t)$  is considered as persistently exciting of a sufficiently high order.

- A3. The additive noises  $n_i(t)$  and  $n_o(t)$  are zero-mean ergodic white processes with *unknown* variances  $\sigma_i^*$  and  $\sigma_o^*$ .
- A4.  $n_i(t)$ ,  $n_o(t)$  and  $x(t)$  are mutually uncorrelated.

Let  $\{u(t)\}_{t=0}^{N-1}$  and  $\{y(t)\}_{t=0}^{N-1}$  be a set of input and output observations at  $N$  equidistant time instants. For  $\{u(t)\}_{t=0}^{N-1}$ , the corresponding Discrete Fourier Transform (DFT) is defined as

$$U(\omega_k) = \frac{1}{\sqrt{N}} \sum_{t=0}^{N-1} u(t) e^{-j\omega_k t} \quad (6)$$

where  $\omega_k = 2\pi k/N$  and  $k = 0, \dots, N-1$ . Similarly, let  $Y(\omega_k)$  be the DFT of  $\{y(t)\}_{t=0}^{N-1}$ . In the frequency domain, the problem under investigation can be stated as follows.

*Problem 1.* Let  $U(\omega_k)$ ,  $Y(\omega_k)$  be a set of noisy measurements generated by a FIR system of type (1)–(4), under Assumptions A1–A4. Estimate the system parameters  $h_i$  ( $i = 0, \dots, M-1$ ) and the noise variances  $\sigma_i^*$ ,  $\sigma_o^*$ .

*Remark 1.* For real-valued signals, the following consideration holds for every  $N$ , even or odd. Let  $s(t)$  denote either  $u(t)$  or  $y(t)$ . It can be observed that for  $k = 0, \dots, \text{floor}(\frac{N}{2})$

$$\begin{aligned} S(\omega_{N-1-k}) &= \frac{1}{\sqrt{N}} \sum_{t=0}^{N-1} s(t) e^{-j \frac{N-1-k}{N} 2\pi t} \\ &= \frac{1}{\sqrt{N}} \sum_{t=0}^{N-1} s(t) e^{-j \frac{-(1+k)}{N} 2\pi t} = \bar{S}(\omega_{1+k}), \end{aligned} \quad (7)$$

where  $\bar{S}(\cdot)$  is the complex conjugate of  $S(\cdot)$ . Thus, a redundant information is used when the full data set is considered. In fact, it is worth observing that the two algorithms proposed in the Sections 5 and 6 yield consistent estimates of the system parameters by using only the first  $N_{\text{half}} = \text{ceil}((N+1)/2)$  samples  $U(\omega_k)$ ,  $Y(\omega_k)$ ,  $k = 0, \dots, \text{floor}(\frac{N}{2})$ , see also Remark 5.

## 3. A FREQUENCY DOMAIN SETUP

In this section a new frequency domain description for the noisy FIR model (1)–(4) is introduced. This setup has been originally developed in [29; 30] with reference to the identification of errors-in-variables systems. In this respect, the maximum likelihood solution has been analyzed in depth in [27].

### 3.1 The noise-free case

Similarly to equation (6), let  $X(\omega_k)$  and  $D(\omega_k)$  be the DFTs of the signals  $x(t)$  and  $d(t)$  appearing in equation (1). It is a well-known fact [16; 19] that for finite  $N$ , even in absence of noise, the DFTs  $X(\omega_k)$  and  $D(\omega_k)$  exactly satisfy an extended model that includes also a transient term, i.e.

$$D(\omega_k) = H(e^{-j\omega_k})X(\omega_k) + T(e^{-j\omega_k}), \quad (8)$$

where  $T(z^{-1})$  is a polynomial of order  $M-2$

$$T(z^{-1}) = \tau_0 + \tau_1 z^{-1} + \dots + \tau_{M-2} z^{-M+2} \quad (9)$$

that takes into account the effects of the initial and final conditions of the experiment.

By considering the whole number of frequencies, eq. (8) can be rewritten in a matrix form. For this purpose, introduce the parameter vectors

$$h = [h_0 \ h_1 \ \dots \ h_{M-1}]^T \quad (10)$$

$$h_\tau = [\tau_0 \ \dots \ \tau_{M-2}]^T \quad (11)$$

and define the following vector

$$\Theta = [1 \ -h^T \ -h_\tau^T]^T, \quad (12)$$

with dimension

$$p = 2M. \quad (13)$$

In absence of noise, the parameter vector (12) can be recovered by means of the following procedure. Define the row vectors

$$Z_M(\omega_k) = [1 \ e^{-j\omega_k} \ \dots \ e^{-j(n-1)\omega_k} \ e^{-j(M-1)\omega_k}] \quad (14)$$

$$Z_{M-1}(\omega_k) = [1 \ e^{-j\omega_k} \ \dots \ e^{-j(M-2)\omega_k}], \quad (15)$$

whose entries are constructed with multiple frequencies of  $\omega_k$ , and construct the following matrices

$$\Pi = \begin{bmatrix} Z_M(\omega_0) \\ \vdots \\ Z_M(\omega_{N-1}) \end{bmatrix} \quad \Psi = \begin{bmatrix} Z_{M-1}(\omega_0) \\ \vdots \\ Z_{M-1}(\omega_{N-1}) \end{bmatrix} \quad (16)$$

of dimension  $N \times M$  and  $N \times (M-1)$ , respectively.

Using the DFT samples  $D(\omega_k)$  and  $X(\omega_k)$  construct the following  $N \times N$  diagonal matrix

$$V_X^{diag} = \text{diag}[X(\omega_0), X(\omega_1), \dots, X(\omega_{N-1})] \quad (17)$$

and the  $N$ -dimensional column vector

$$V_D = [D(\omega_0), D(\omega_1), \dots, D(\omega_{N-1})]^T. \quad (18)$$

Then, compute the  $N \times M$  matrix

$$\Phi_X = V_X^{diag} \Pi \quad (19)$$

and construct the  $N \times p$  matrix

$$\hat{\Phi} = [V_D | \Phi_X | \Psi]. \quad (20)$$

Thus, eq. (8) for  $k = 0, \dots, N - 1$  can be rewritten as

$$\hat{\Phi} \Theta = 0. \quad (21)$$

It then holds

$$\hat{\Sigma} \Theta = 0, \quad (22)$$

where  $\hat{\Sigma}$  is the  $p \times p$  matrix

$$\hat{\Sigma} = \frac{1}{N} (\hat{\Phi}^H \hat{\Phi}), \quad (23)$$

and  $(\cdot)^H$  denotes the transpose and conjugate operation.

*Remark 2.* Since  $d(t)$  is generated by the FIR model (1), the relation (8) cannot be satisfied by a polynomial  $H(z^{-1})$  with order lower than  $M - 1$ . Therefore, the matrix  $\hat{\Sigma}$  in (23) is positive semidefinite, with only one null eigenvalue, i.e.

$$\hat{\Sigma} \geq 0 \quad \dim \ker \hat{\Sigma} = 1. \quad (24)$$

*Remark 3.* If the signals  $x(t)$  and  $d(t)$  happen to be  $N$ -periodic, then the term  $T(e^{-j\omega h})$  in equation (8) is identically zero. In this case, the matrix in (20) can be reduced to the  $N \times (M + 1)$  matrix

$$\hat{\Phi}_{per} = [V_D | \Phi_X]. \quad (25)$$

It then holds

$$\hat{\Sigma}_{per} \theta = 0, \quad (26)$$

where  $\hat{\Sigma}_{per}$  is the  $(M + 1) \times (M + 1)$  positive semidefinite matrix

$$\hat{\Sigma}_{per} = \frac{1}{N} (\hat{\Phi}_{per}^H \hat{\Phi}_{per}) \quad (27)$$

and  $\theta$  is the  $M + 1$  parameter vector

$$\theta = [1 - h^T]^T. \quad (28)$$

In the following it will be shown how it is possible to reorganize the equations as they would have been generated by a periodic system, for every value of  $N$ .

Partition the matrix  $\hat{\Sigma}$ , defined in (23), as follows

$$\hat{\Sigma} = \begin{bmatrix} \hat{\sigma}_{11} & \hat{\Sigma}_{12} & \hat{\Sigma}_{13} \\ \hat{\Sigma}_{21} & \hat{\Sigma}_{22} & \hat{\Sigma}_{23} \\ \hat{\Sigma}_{31} & \hat{\Sigma}_{32} & \hat{\Sigma}_{33} \end{bmatrix}, \quad (29)$$

where  $\hat{\sigma}_{11}$  is a scalar,  $\hat{\Sigma}_{22}$  is a square matrix of dimension  $M$  and  $\hat{\Sigma}_{33}$  is a square matrix of dimension  $M - 1$ . Relation (22) can be expanded as follows

$$\hat{\sigma}_{11} - \hat{\Sigma}_{12} h - \hat{\Sigma}_{13} h_\tau = 0 \quad (30)$$

$$\hat{\Sigma}_{21} - \hat{\Sigma}_{22} h - \hat{\Sigma}_{23} h_\tau = 0 \quad (31)$$

$$\hat{\Sigma}_{31} - \hat{\Sigma}_{32} h - \hat{\Sigma}_{33} h_\tau = 0. \quad (32)$$

From (32) we obtain

$$h_\tau = \hat{\Sigma}_{33}^{-1} (\hat{\Sigma}_{31} - \hat{\Sigma}_{32} h). \quad (33)$$

The expression (33) can then be substituted into (30) and (31). Defining the following matrices

$$\hat{\Sigma}_{red} = \begin{bmatrix} \hat{\sigma}_{11} & \hat{\Sigma}_{12} \\ \hat{\Sigma}_{21} & \hat{\Sigma}_{22} \end{bmatrix} \quad \hat{T} = \begin{bmatrix} \hat{\Sigma}_{13} \hat{\Sigma}_{33}^{-1} \hat{\Sigma}_{31} & \hat{\Sigma}_{13} \hat{\Sigma}_{33}^{-1} \hat{\Sigma}_{32} \\ \hat{\Sigma}_{23} \hat{\Sigma}_{33}^{-1} \hat{\Sigma}_{31} & \hat{\Sigma}_{23} \hat{\Sigma}_{33}^{-1} \hat{\Sigma}_{32} \end{bmatrix} \quad (34)$$

it is possible to reduce the non-periodic case into an equivalent periodic one, with lower dimensions (cf. (26))

$$\hat{\Sigma}_{per} = \hat{\Sigma}_{red} - \hat{T} \quad (35)$$

$$\hat{\Sigma}_{per} \theta = 0, \quad (36)$$

where  $\theta$  has been defined in (28).

For noise-free data, the ratio

$$\hat{\rho} = \frac{\|\hat{T}\|_F}{\|\hat{\Sigma}_{red}\|_F} \quad (37)$$

can give a measure of the effect of the transient term, where  $\|\cdot\|_F$  is the Frobenius norm of a matrix.

*Remark 4.* Given the input sequence  $x(t)$ , the ratio  $\hat{\rho}$  takes into account both the parameters and the order of the FIR system. Note that  $\hat{\rho}$  is a function of the data length  $N$ . In particular,  $\hat{\rho} \rightarrow 0$  if  $N \rightarrow \infty$ , and

$$\hat{\rho}_{max} = \hat{\rho}(N_{min}), \quad (38)$$

where  $N_{min} = 2M - 1$  is the minimum length of the input-output sequence, i.e. the minimum number of equations so that relation (24) holds.

### 3.2 The noisy case

In the presence of noise, the previous considerations can be modified as follows. With the noisy input-output DFT samples  $U(\omega_k)$ ,  $Y(\omega_k)$  construct the  $N \times N$  diagonal matrix

$$V_U^{diag} = \text{diag}[U(\omega_0), U(\omega_1), \dots, U(\omega_{N-1})] \quad (39)$$

and the  $N$ -dimensional column vector

$$V_Y = [Y(\omega_0), Y(\omega_1), \dots, Y(\omega_{N-1})]^T. \quad (40)$$

Then, compute the matrix

$$\Phi_U = V_U^{diag} \Pi \quad (41)$$

and construct the  $N \times p$  matrix

$$\Phi = [V_Y | \Phi_U | \Psi]. \quad (42)$$

Because of Assumptions A3-A4, when  $N \rightarrow \infty$ , we obtain the following  $p \times p$  positive definite matrix

$$\Sigma = \frac{1}{N} (\Phi^H \Phi) = \hat{\Sigma} + \tilde{\Sigma}^*, \quad (43)$$

where

$$\tilde{\Sigma}^* = \begin{bmatrix} \sigma_o^* & 0 & 0 \\ 0 & \sigma_i^* I_M & 0 \\ 0 & 0 & 0_{M-1} \end{bmatrix}. \quad (44)$$

From (12), (22) and (43), the parameter vector  $\Theta$ , defined in (12), can be obtained as the kernel of

$$(\Sigma - \tilde{\Sigma}^*) \Theta = 0, \quad (45)$$

after normalizing the first entry of  $\Theta$  to 1.

*Remark 5.* The previous considerations hold also when only a subset of the whole frequency range is used, i.e.  $\omega_k \in W = [\omega_i, \omega_f]$ , with  $i \geq 0$  and  $f \leq \text{floor}(\frac{N}{2})$ , containing  $L = f - i + 1$  frequencies. The subset  $W$  must be chosen by the user on the basis of *a priori* knowledge of the frequency properties of the FIR system and of the noise-free input  $X(\omega_k)$ . The choice of  $W = [\omega_i, \omega_f]$  reduces the number of the entries in (16) and (39)-(40), and all the related equations must be

consequently modified. Some care must be used when the algorithms of Sections 5 and 6 make use of the whole DFT data set  $U(\omega_k)$ ,  $Y(\omega_k)$ ,  $k = 0, \dots, N-1$  [31]. In this case, two distinct sets of frequencies must be jointly considered, the set  $W_1 = [\omega_i, \omega_f]$ , with  $i \geq 0$  and  $f \leq \text{floor}(\frac{N}{2})$  and the set  $W_2 = [\omega_{N-1-f}, \omega_{N-1-i}]$ . The total number of frequencies used in the algorithms will be  $2L$ . By considering a new matrix  $\Phi$  with  $2L$  rows, expressions (43)–(44) must be modified as follows

$$\Sigma = \frac{1}{2L} (\Phi^H \Phi) = \hat{\Sigma} + \tilde{\Sigma}^*, \quad (46)$$

where

$$\tilde{\Sigma}^* = \frac{N}{2L} \begin{bmatrix} \sigma_o^* & 0 & 0 \\ 0 & \sigma_i^* I_M & 0 \\ 0 & 0 & 0_{M-1} \end{bmatrix}. \quad (47)$$

*Remark 6.* The noise Assumptions A3–A4 are necessary in order to obtain a diagonal matrix  $\tilde{\Sigma}^*$ , as defined in (44), when  $N \rightarrow \infty$ . On the other hand, one can observe that for large  $N$  the effect of the transient polynomial  $T(z^{-1})$  is negligible since it vanishes with order  $O(1/\sqrt{N})$  [18] and the data could be treated as periodic, as done in Remark 3. This is a common procedure used in many frequency domain identification approaches, see e.g. [13; 22].

An alternative solution is to proceed as in Section 3.1. Partition the matrix  $\Sigma$ , defined in (43), according to the matrix  $\hat{\Sigma}$  in equation (29). Expanding relation (45) as in (30)–(31), we obtain

$$\hat{\sigma}_{11} - \Sigma_{12} h - \Sigma_{13} h_\tau = 0 \quad (48)$$

$$\Sigma_{21} - \hat{\Sigma}_{22} h - \Sigma_{23} h_\tau = 0 \quad (49)$$

$$\Sigma_{31} - \Sigma_{32} h - \Sigma_{33} h_\tau = 0. \quad (50)$$

Next (50) implies

$$h_\tau = \Sigma_{33}^{-1} (\Sigma_{31} - \Sigma_{32} h). \quad (51)$$

Substitute now the expression (51) in (48)–(49), define the matrices

$$\Sigma_{red} = \begin{bmatrix} \sigma_{11} & \Sigma_{12} \\ \Sigma_{21} & \Sigma_{22} \end{bmatrix}, \quad T = \begin{bmatrix} \Sigma_{13} \Sigma_{33}^{-1} \Sigma_{31} & \Sigma_{13} \Sigma_{33}^{-1} \Sigma_{32} \\ \Sigma_{23} \Sigma_{33}^{-1} \Sigma_{31} & \Sigma_{23} \Sigma_{33}^{-1} \Sigma_{32} \end{bmatrix} \quad (52)$$

and set

$$R = \Sigma_{red} - T. \quad (53)$$

Defining the matrix

$$\tilde{R}^* = \begin{bmatrix} \sigma_o^* & 0 \\ 0 & \sigma_i^* I_M \end{bmatrix}, \quad (54)$$

it is then possible to derive the system of equations (cf. (36))

$$(R - \tilde{R}^*) \theta = 0. \quad (55)$$

Also in this case, the ratio

$$\rho = \frac{\|T\|_F}{\|\Sigma_{red}\|_F} \quad (56)$$

can give a measure of the effect of the transient term, starting from the available noisy data.

*Remark 7.* Simulation experiences have shown that, for every value of  $N$ ,  $\rho > \hat{\rho}$  holds, and the effect of the noise

$$\delta = \frac{\rho - \hat{\rho}}{\hat{\rho}} \quad (57)$$

decreases as the amount of noise decreases (see Figure 2). Since the ratio  $\hat{\rho}$  is greater when the number of data  $N$  is shorter, the effect of the transient term is of major importance in the

system parameter estimates when the data sequences are short and affected by a small amount of noise.

## 4. DISCUSSION OF SOME EIV CONTEXTS

### 4.1 The GIVE framework

Note that (55) consists of  $M+1$  algebraic non-linear equations. The number of unknowns is  $M+2$ , i.e. the elements of  $h$  in (10) and the two variances  $\sigma_o^*$  and  $\sigma_i^*$ . In the time domain, a similar set of equations has been largely studied in the identification of EIV dynamic systems. A general framework has been originally introduced in [23], where the Generalized Instrumental Variable Estimation (GIVE) method was proposed with reference to SISO EIV systems affected by additive white noises. The method has been generalized to the case of correlated measurement noises in [25]. The GIVE method provides a unique general framework for the whole class of bias-compensating methods, including iterative solutions, like the BELS methods [26]. The GIVE frameworks leads to the following conclusions, that are common to the whole class of bias-compensating methods.

- 1 Since the number of the unknowns is larger than the number of equations, some further equations need to be used in addition to the system (55) in order to find a unique estimate of  $\theta$ . It can result in an over-determined system of equations. In the time domain, a natural solution is to exploit the high-order Yule-Walker equations, where the noise variances are not present. Indeed, these are the equations exploited also by two methods proposed in this paper. In Section 5 we will see how these equations can be written in the frequency domain.
- 2 In the general case the parameter estimates are obtained as the solution of an optimization problem. An usual solution strategy consists in forcing some of the over-determined system of equations to hold exactly, while the others are minimized in a weighted least squares sense.
- 3 This second aspect does not affect the statistical properties of the estimates, since the asymptotic accuracy depends only on the set of equations used to define the problem and not on the way the equations are solved [26]. Nevertheless, in practice, different identification algorithms that are based on the same set of equations can lead to different estimation results, in terms of computational complexity and speed of convergence. In particular, it will be shown that the over-determined systems of equations exploited by the two proposed methods differ only for one equation, but the way they are solved is completely different.

### 4.2 The Frisch scheme context

The purpose of this subsection is to exploit some properties of the Frisch scheme [2; 9; 24] for developing the estimation algorithm of Section 5. This can be thought as a possible numerical strategy to solve the ‘exact’ equations within the GIVE framework, as stated in the point 2.

Starting from an assumed knowledge of the noisy matrix  $R$  in (53), the determination of the system parameter vector  $\theta$  and of the noise variances  $\sigma_i^*$ ,  $\sigma_o^*$  in eq. (55) can be seen as a Frisch scheme problem. This problem can be solved both in the time and in the frequency domain. In fact, the properties of the locus of the solutions in the noise plane  $\mathcal{R}^2$  are the same. An in-depth description of these properties can be found in [2; 9; 24].

In the following we recall the main results. For the reader's convenience the proofs are reported in the appendix.

Consider the set of non-negative definite diagonal matrices of type

$$\tilde{R} = \text{diag} [\sigma_o, \sigma_i I_M] \quad (58)$$

such that

$$R - \tilde{R} \geq 0 \quad \det(R - \tilde{R}) = 0, \quad (59)$$

and partition the positive definite matrix  $R$  as follows

$$R = \begin{bmatrix} r_{11} & R_{12} \\ R_{21} & R_{22} \end{bmatrix}, \quad (60)$$

where  $r_{11}$  is a scalar and  $R_{22}$  is a square matrix of dimension  $M$ .

*Theorem 1.* The maximal admissible value of the input noise variance  $\sigma_i^{max}$  compatible with the conditions (59) is obtained when  $\sigma_o = 0$  and is given by

$$\sigma_i^{max} = \min \text{eig} \left( R_{22} - \frac{R_{21} R_{12}}{r_{11}} \right). \quad (61)$$

Similarly, the maximal admissible value of the output noise variance  $\sigma_o^{max}$  compatible with the conditions (59) is obtained when  $\sigma_i = 0$  and is given by

$$\sigma_o^{max} = r_{11} - R_{12} R_{22}^{-1} R_{21} = \frac{\det(R)}{\det(R_{22})}. \quad (62)$$

*Theorem 2.* The set of all matrices  $\tilde{R}$  satisfying the conditions (59) defines the points  $P = (\sigma_i, \sigma_o)$  of a continuous curve  $\mathcal{S}(R)$  belonging to the first quadrant of the noise space  $\mathcal{R}^2$ .

*Theorem 3.* The curve  $\mathcal{S}(R)$  defined in *Theorem 2* describes a convex set in the first quadrant of  $\mathcal{R}^2$ , whose concavity faces the origin.

As an immediate consequence of the two previous theorems, we have the following corollary.

*Corollary 1.* Every point  $P = (\sigma_i, \sigma_o)$  of  $\mathcal{S}(R)$  can be associated with a noise matrix of type  $\tilde{R}(P)$  (58) and with a coefficient vector  $\theta(P)$ , satisfying the relation

$$(R - \tilde{R}(P)) \theta(P) = 0. \quad (63)$$

Asymptotically, when  $N \rightarrow \infty$ , thanks to the relations (55) and (54), the following corollary can be stated.

*Corollary 2.* When  $N \rightarrow \infty$ , the point  $P^* = (\sigma_i^*, \sigma_o^*)$ , associated with the true variances of  $n_i(t)$  and  $n_o(t)$ , belongs to  $\mathcal{S}(R)$  and the corresponding coefficient vector  $\theta(P^*)$  is characterized (after a normalization of its first entry to 1) by the true system parameter vector, i.e.  $\theta(P^*) = \theta$ .

The next theorem describes a parametrization of the curve  $\mathcal{S}(R)$  that allows to associate a solution of (59) with every straight line departing from the origin and lying in the first quadrant [9]. This parametrization plays an important role in the practical implementation of the identification algorithm.

*Theorem 4.* Let  $\xi = (\xi_1, \xi_2)$  be a generic point of the first quadrant of  $\mathcal{R}^2$  and  $r$  the straight line from the origin through  $\xi$ . Its intersection with  $\mathcal{S}(R)$  is the point  $P = (\sigma_i, \sigma_o)$  given by

$$\sigma_i = \frac{\xi_1}{\lambda_M} \quad \sigma_o = \frac{\xi_2}{\lambda_M}, \quad (64)$$

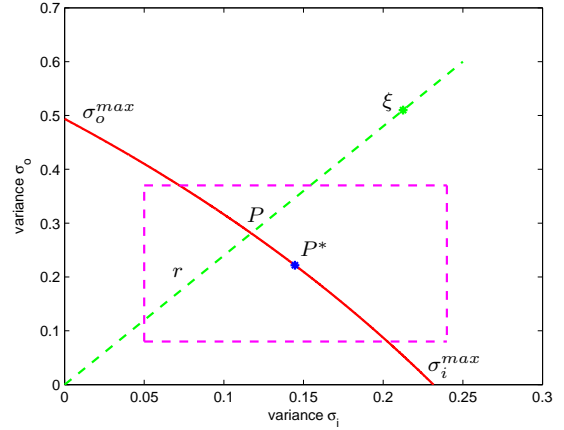


Fig. 1. Typical shape of  $\mathcal{S}(R)$

where

$$\lambda_M = \max \text{eig} (R^{-1} \tilde{R}_\xi) \quad (65)$$

$$\tilde{R}_\xi = \begin{bmatrix} \xi_2 & 0 \\ 0 & \xi_1 I_M \end{bmatrix}. \quad (66)$$

The described procedure allows to construct the curve  $\mathcal{S}(R)$  in the noise space  $(\sigma_i, \sigma_o)$ . As an example, Figure 1 reports the curve  $\mathcal{S}(R)$  of the numerical Example 1 of Section 8.

*Remark 8.* In many practical situations it is possible to have some information about the lower and upper bounds of the noise covariances  $\sigma_i^*$  and  $\sigma_o^*$ , for example when other measurements taken in different experimental conditions are available. In these cases, the search of the point  $P^*$  on the curve  $\mathcal{S}(R)$  can be bounded within a limited area in the noise plane  $\mathcal{R}^2$ , e.g. see the box depicted in Figure 1.

## 5. A CRITERION BASED ON HOYW-TYPE EQUATIONS

As stated in Theorem 2, the determination of the point  $P^*$  on  $\mathcal{S}(R)$  leads to the solution of Problem 1. Unfortunately, the theoretic properties of  $\mathcal{S}(R)$  described so far do not allow to distinguish point  $P^*$  from the other points of the curve. Some additional condition must be added to define a unique estimate.

In this section we will describe a possible search criterion. This criterion is analogue to that reported in [31] with reference to frequency domain identification of EIV systems.

Select the integer  $q \geq 2M - 1$ . The value of the parameter  $q$  is a user choice. In general, this value can affect the quality of the estimates. A good choice, from simulation experience, is  $q = 2M - 1$ . Analogously to (14), consider the row vector

$$Z_{q+M}(\omega_k) = [1 e^{-j\omega_k} \dots e^{-j(M-1+q)\omega_k}] \quad (67)$$

and extract from it the  $q$ -dimensional row vector

$$Z_q^h(\omega_k) = [e^{-jM\omega_k} \dots e^{-j(M-1+q)\omega_k}]. \quad (68)$$

Then, construct the following  $N \times q$  matrix

$$\Pi^h = \begin{bmatrix} Z_q^h(\omega_0) \\ \vdots \\ Z_q^h(\omega_{N-1}) \end{bmatrix}. \quad (69)$$

and compute the  $N \times q$  matrix

$$\hat{\Phi}^h = V_X^{diag} \Pi^h. \quad (70)$$

Define now the  $q \times p$  matrix

$$\hat{\Sigma}^h = \frac{1}{N} ((\hat{\Phi}^h)^H \hat{\Phi}). \quad (71)$$

Because of (21) we have

$$\hat{\Sigma}^h \Theta = 0. \quad (72)$$

In an analogous way, in the noisy case, we can compute the  $N \times q$  matrix

$$\Phi^h = V_U^{diag} \Pi^h \quad (73)$$

and define the  $q \times p$  matrix

$$\Sigma^h = \frac{1}{N} ((\Phi^h)^H \Phi). \quad (74)$$

Because of Assumptions A3–A4, when  $N \rightarrow \infty$  it results

$$\Sigma^h = \hat{\Sigma}^h. \quad (75)$$

It is thus possible to write

$$\Sigma^h \Theta = 0. \quad (76)$$

It is not difficult to show that the dimensions of equation (76) can be reduced. For this purpose, partition matrix  $\Sigma^h$  as follows

$$\Sigma^h = [\Sigma_1^h \ \Sigma_2^h \ \Sigma_3^h], \quad (77)$$

where the matrices  $\Sigma_1^h, \Sigma_2^h, \Sigma_3^h$  have dimensions  $q \times 1, q \times M, q \times (M-1)$ , respectively. Thanks to (51), equation (76) can be reduced to

$$R^h \theta = 0, \quad (78)$$

where  $\theta$  has been defined in (28) and

$$R^h = [\Sigma_1^h - \Sigma_3^h \Sigma_{33}^{-1} \Sigma_{31} \ \Sigma_2^h - \Sigma_3^h \Sigma_{33}^{-1} \Sigma_{32}]. \quad (79)$$

*Remark 9.* Equation (76) constitutes a set of  $q$  equations, analogue to the time domain high order Yule–Walker equations, that does not involve the noise variances  $\sigma_i^*, \sigma_o^*$ . These equations could be directly used to obtain an estimate of the parameter vector  $\Theta$  if  $q \geq 2M-1$ .

*Remark 10.* Equation (76) are analogue to an instrumental variable (IV) method in the time domain, where delayed outputs are used as instruments. These equations can be solved by using a total least squares approach. The main advantage of the method is the computational efficiency. On the other hand, the obtained estimation precision is often poor [24].

*Remark 11.* The set of  $(M+1)$  non-linear equations (55) can be joined to the set of  $q$  linear equations (78), with  $q \geq 2M-1$  and can be settled within the GIVE framework, as described in Subsection 4.1. Thus, the results in [23] and [24] can be applied, to express the statistical accuracy in terms of the theoretical asymptotic covariance matrix of the parameter estimates. More precisely, applying the Frisch scheme described in Subsection 4.2, the equations (55) are treated as a constraint that must be exactly satisfied, while the equations (78) must hold approximately. In other words, the search for  $P^*$  along  $\mathcal{S}(R)$  can be performed by minimizing a quadratic cost function.

The result of Theorem 4 allows to move radially on  $\mathcal{S}(R)$ . For every point  $P$  on  $\mathcal{S}(R)$ , one can compute the parameter vector  $\theta(P)$  defined in (63) and evaluate the cost function

$$J(P) = \|R^h \theta(P)\|_2^2 = \theta^T(P) (R^h)^H R^h \theta(P), \quad (80)$$

which exhibits the following properties

$$\text{i) } J(P) \geq 0 \quad \text{ii) } J(P) = 0 \Leftrightarrow P = P^*.$$

In general, for a finite number of data, the minimum of  $J(P)$  will not be exactly obtained for  $P = P^*$ .

On the basis of the previous considerations, the following algorithm can be developed.

*Algorithm 1.*

- (1) Compute, on the basis of the available time domain data, the DFTs  $U(\omega_k), Y(\omega_k)$ , as defined in (6).
- (2) Compute the matrix  $\Phi_U$  as in (41) and construct the matrix  $\Phi$  as in (42).
- (3) Compute, as in (43), the sample estimate of the matrix

$$\Sigma = \frac{1}{N} (\Phi^H \Phi) \quad (81)$$

and compute the matrix  $R$  by means of (53).

- (4) Select  $q \geq 2M-1$  and construct the matrix  $\Pi^h$  as in (69), then compute  $\Phi^h$  as in (73).
- (5) Compute, as in (74), the sample estimate of the matrix

$$\Sigma^h = \frac{1}{N} ((\Phi^h)^H \Phi) \quad (82)$$

and compute the matrix  $R^h$  by means of (79).

- (6) Start from a generic point  $\xi$  (a generic direction) in the first quadrant of  $\mathcal{R}^2$  and compute, by means of (64)–(66) the corresponding point  $P = (\sigma_i, \sigma_o)$  on  $\mathcal{S}(R)$ .
- (7) Compute the estimates of  $\hat{R}(P)$  and  $\theta(P)$  by means of the relations

$$\hat{R}(P) = R - \text{diag}[\sigma_o, \sigma_i I_M], \quad (83)$$

$$\hat{R}(P) \theta(P) = 0. \quad (84)$$

- (8) Compute the value of the cost function  $J(P)$  (80).
- (9) Search on the curve  $\mathcal{S}(R)$  for the point associated with the minimum of  $J(P)$ .

*Remark 12.* The Algorithm 1 makes reference to  $N$  data. As observed in Remark 1, if only  $N_{\text{half}} = \text{ceil}(\frac{N+1}{2})$  data are considered, the algorithm must be modified in a straightforward fashion, by substituting  $N$  with  $N_{\text{half}}$ , starting from step (2).

## 6. A SUBSPACE APPROACH

The approach proposed in this section is analogue to that described in [4] for the identification of autoregressive models affected by additive noise. This alternative method is not directly based on the Frisch scheme, but exploits the set of equations (76) together with the equations (45). It will be shown that the FIR plus noise identification problem can be mapped into a quadratic eigenvalue problem that, in turn, can be solved as a generalized eigenvalue problem. The principle has been applied to some other identification problems as well [5; 32].

Consider again equation (45), expanded as in (48)–(50). The last  $2M-1$  equations (49)–(50) can be written as

$$\begin{bmatrix} \Sigma_{21} & \Sigma_{22} - \sigma_i^* I_M & \Sigma_{23} \\ \Sigma_{31} & \Sigma_{32} & \Sigma_{33} \end{bmatrix} \Theta = 0. \quad (85)$$

Equation (85) contains  $2M+1$  unknowns, i.e.  $\sigma_i^*$  and the entries of  $\Theta$ . The equations (76) can be combined with the equations (85) in order obtain the following nonlinear system of  $2M-1+q$  equations

$$\begin{bmatrix} \Sigma_{21} & \Sigma_{22} - \sigma_i^* I_M & \Sigma_{23} \\ \Sigma_{31} & \Sigma_{32} & \Sigma_{33} \\ & \Sigma^h & \end{bmatrix} \Theta = 0. \quad (86)$$

It can be observed that the dimensions of the equation (86) can be reduced. For this purpose, consider the matrix  $R$  defined in (53) and rewritten with the notation introduced in (60). Moreover, consider the matrix  $R^h$  defined in (79). Thanks to (51), equation (86) can be reduced to

$$\begin{bmatrix} R_{21} & R_{22} - \sigma_i^* I_M \\ & R^h \end{bmatrix} \theta = 0. \quad (87)$$

*Remark 13.* Observe that the set of equations (87) differ from the set of equations (55) and (78) by only one equation, in fact the first row in (55) is missing. Also the set of equations (87) can be settled within the GIVE framework of Subsection 4.1. As shown in the following, all the equations (87) are minimized in a total least squares sense, by solving a minimal eigenvalue problem. Of course, the asymptotic analysis proposed in [23] and [24] can be applied also in this case.

The equations (87) can be compactly rewritten as

$$(S - \sigma_i^* J) \theta = 0, \quad (88)$$

where

$$S = \begin{bmatrix} R_{21} & R_{22} \\ R^h & \end{bmatrix} \quad J = \begin{bmatrix} 0_{M \times 1} & I_M \\ 0_{q \times (M+1)} & \end{bmatrix}. \quad (89)$$

Equations (89) represent a non-square generalized eigenvalue problem. In order to solve it, in the following we pursue the approach proposed in [4].

Multiplying both sides of (88) by  $(S - \sigma_i^* J)^T$  leads to the equation

$$(A_2 \sigma_i^{2*} + A_1 \sigma_i^* + A_0) \theta = 0, \quad (90)$$

where

$$A_0 = S^T S \quad A_1 = -(S^T J + J^T S) \quad A_2 = J^T J. \quad (91)$$

The  $M + 1$  coefficients of  $\theta$  can thus be estimated by solving the following quadratic eigenvalue problem (QEP)

$$(A_2 \lambda^2 + A_1 \lambda + A_0) v = 0. \quad (92)$$

Equations (92) can be solved by rewriting them as

$$A_2 v' \lambda + A_1 v \lambda + A_0 v = 0, \quad (93)$$

where  $v' = \lambda v$ . Thus, the following  $(2M + 2)$ -dimensional generalized eigenvalue problem can be derived

$$(P - \lambda Q) \eta = 0, \quad (94)$$

where

$$P = \begin{bmatrix} A_0 & 0 \\ 0 & I_{M+1} \end{bmatrix} \quad Q = \begin{bmatrix} -A_1 & -A_2 \\ I_{M+1} & 0 \end{bmatrix} \quad \eta = \begin{bmatrix} v \\ v' \end{bmatrix}. \quad (95)$$

Following the discussion of [4], it can be stated that, asymptotically when the the number of data  $N \rightarrow \infty$ , the only real-valued eigenvalue solving (94) is  $\sigma_i^*$  and the first  $M + 1$  entries of the corresponding eigenvector  $\eta^*$  are, after a normalization of the first entry to 1, the entries of  $\theta$ , i.e.

$$\eta_0 = \frac{\eta^*}{\eta^*(1)} = [\theta^T \quad \sigma_i^* \theta^T]^T. \quad (96)$$

*Remark 14.* Since only a finite number  $N$  of data is available, all the eigenvalues solving (94) will exhibit, in general, a small imaginary part. A criterion leading to good results consists in choosing the eigenvalue having the smallest modulus [4].

The whole identification procedure can be summarized as follows.

*Algorithm 2.*

- (1) Compute, on the basis of the available time domain data, the DFTs  $U(\omega_k)$ ,  $Y(\omega_k)$ , as defined in (6).
- (2) Compute the matrix  $\Phi_U$  as in (41) and construct the matrix  $\Phi$  as in (42).
- (3) Compute, as in (43), the sample estimate of matrix

$$\Sigma = \frac{1}{N} (\Phi^H \Phi) \quad (97)$$

and compute the matrix  $\Sigma_r$  by means of (53).

- (4) Select  $q \geq 2M - 1$  and construct the matrix  $\Pi^h$  as in (69), then compute  $\Phi^h$  as in (73).
- (5) Compute, as in (74), the sample estimate of matrix

$$\Sigma^h = \frac{1}{N} ((\Phi^h)^H \Phi) \quad (98)$$

and compute the matrix  $R^h$  by means of (79).

- (6) Construct the matrices  $S$  and  $J$  as in (89) and compute the matrices  $A_0, A_1, A_2$  (91).
- (7) Construct the matrices  $P$  and  $Q$  as in (95).
- (8) Solve the generalized eigenvalue problem

$$(P - \lambda Q) \eta = 0 \quad (99)$$

and choose as estimate of  $\sigma_i^*$  the modulus of the generalized eigenvalue having minimum modulus. Let  $\eta^*$  be the corresponding eigenvector.

- (9) Divide  $\eta^*$  by the first entry  $\eta^*(1)$  in order to obtain an estimate of  $\theta$ , as in (96)

$$\eta_0 = [\theta^T \quad \#]^T, \quad (100)$$

where  $\#$  denotes the last  $M + 1$  entries of  $\eta^*/\eta^*(1)$ , which are not of interest.

- (10) Consider the first equation in (55)

$$[r_{11} - \sigma_o^* R_{12}] \theta = 0 \quad (101)$$

and solve it with respect to the unknown  $\sigma_o^*$ .

## 7. GENERAL CONSIDERATIONS

### 7.1 Estimation of the model order

A possible method for estimating the order  $M - 1$  of the FIR model (1) can be developed on the basis of the following observation. In the time domain, the process

$$e(t) = y(t) - H(z^{-1}) u(t) \quad (102)$$

describes the equation error of the FIR model (1)–(4). By substituting the relations (3) and (4) in (102), we obtain the alternative representation

$$e(t) = n_o(t) - H(z^{-1}) n_i(t). \quad (103)$$

Because of Assumptions A3-A4, the equation (103) proves that the equation error  $e(t)$  is an MA process of order  $M - 1$ , whose autocovariance function  $r_e(k) = E[e(t) e(t - k)]$  is given by

$$r_e(0) = \sigma_o^* + \sigma_i^* \sum_{i=0}^{M-1} h_i^2 \quad (104)$$

$$r_e(k) = \sigma_i^* \sum_{i=0}^{M-k-1} h_i h_{i+k} \quad \text{for } k = 1, \dots, M - 1 \quad (105)$$

$$r_e(k) = 0 \quad \text{for } k > M - 1. \quad (106)$$

Thus, a possible way for estimating the order  $M - 1$  of (1) consists in applying one of the proposed algorithms for an increasing sequence of orders  $n$ . Once the parameters  $h_0, \dots, h_n$  of  $H(z^{-1})$  and the variances  $\sigma_o^*, \sigma_i^*$  have been estimated by means of the Algorithm 1 or 2, it is possible to compute the estimates of  $r_e(k)$  by using (104)–(106). The model order  $M - 1$  can be estimated by observing that the cost function

$$J_n = \sum_{k=0}^n r_e(k) \quad n = 1, 2, \dots \quad (107)$$

stabilizes at a constant value for  $n \geq M - 1$ . Note that  $J_n$  represents the value of the spectrum of the MA process  $e(t)$  at zero frequency.



It is worth observing that the Algorithm 1 is to be preferred in the computation of the quantities (104)–(106). In fact, in many cases the Algorithm 2 yields worse estimates of  $\sigma_i^*$ ,  $\sigma_o^*$ .

## 7.2 Practical aspects of frequency filtering

One of the main advantages of the proposed techniques lies in the fact that they allow to perform the identification by using only a reduced number of frequencies, as described in Remark 5. However, this property must be used with some caution, for two main reasons.

First of all, it must be observed that the condition  $q \geq 2M - 1$  of Remark 9, together with Assumption A2, do not assure the consistency of the IV estimate (76). They assure only the “generic consistency”, i.e. the consistency with probability one, see [28] pag. 266. In other words, there may exist cases where the rank of  $\Sigma^h$  in (76) is lower than  $2M - 1$  and consequently the proposed algorithms do not produce consistent estimates. This consideration is particularly important when only a subset of the whole frequency range is used and Assumption A2 may fail.

Moreover, in case of FIR system identification, there is another important aspect that limits the usage of a reduced number of frequencies. The frequency shape of a FIR model is strictly linked with its order, e.g. see [10]. This property has also direct consequences in FIR system identification, as far as the choice of the order is concerned. In fact, from simulation experiences, it is possible to state that, in general, in order to obtain a good identification of the FIR system the model order must be correctly chosen and equal to its nominal value. A choice of a wrong (reduced) model order leads to biased estimates. The previous property is valid also when the system is identified by using a reduced number of frequencies, within a limited window of the spectrum. Also in this case, the order of the identified FIR model  $H(z^{-1})$  must be chosen equal to its nominal value. In the presence of additive white noises on the input and output the previous consideration has a direct consequence. The signal-to-noise ratios of the input and output power spectra are

$$\frac{S_x(\omega_k)}{S_{n_i}(\omega_k)} = \frac{\lim_{N \rightarrow \infty} E[|X(\omega_k)|^2/N]}{\sigma_i^*} \quad (108)$$

$$\frac{S_d(\omega_k)}{S_{n_o}(\omega_k)} = \frac{\lim_{N \rightarrow \infty} E[|D(\omega_k)|^2/N]}{\sigma_o^*} = |H(e^{-j\omega_k})|^2 \frac{\lim_{N \rightarrow \infty} E[|X(\omega_k)|^2/N]}{\sigma_o^*} \quad (109)$$

$$\omega_k = 2\pi k/N \quad k = 0, \dots, N-1.$$

It can be observed that equation (108) is characterized by a constant denominator  $\sigma_i^*$  for all possible frequency windows. Also equation (109) is characterized by a constant denominator  $\sigma_o^*$  for all possible frequency windows since in this case  $H(z^{-1})$  is a transfer function with only zeros, see eq. (2). Thus, restricting the identification within a limited window of the frequency spectrum  $\omega_k \in [\omega_i, \omega_f]$  leads, in general, to worse results with respect to performing the same identification procedure by using the whole set of frequencies, for the simple reason that in the former case the available information of the system  $H(e^{-j\omega_k})$  are only partially exploited. Of course, this consideration is no more valid when the input and output noises are characterized by a spectrum that is not constant for all the frequencies, i.e. when the denominators in the expressions

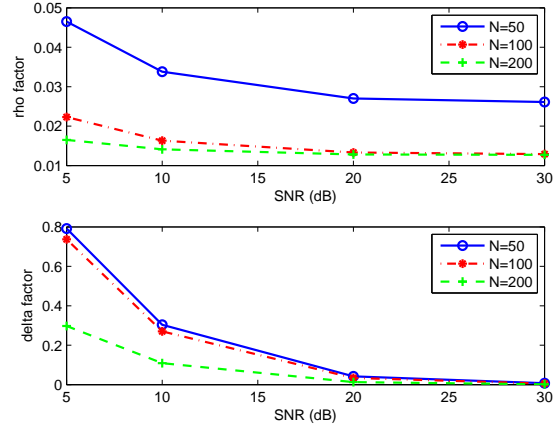


Fig. 2.  $\rho$  and  $\delta$  factors versus SNR.

(108)–(109) are not constant for all the frequency range. In this case the identification of the FIR model by using only a limited number of frequencies can lead to great advantages, if the chosen frequency window is characterized by lower values of the noise spectra.

## 8. NUMERICAL EXAMPLES

The effectiveness of the considered identification algorithms has been tested by means of numerical simulations on several FIR models taken from the literature. As a general consideration, it can be said that quite often the FIR1 algorithm gives better estimates than the FIR2 method, in particular as far as the estimate of the noise variances is concerned.

*Example 1.* The proposed algorithms have been tested on sequences generated by the following FIR model, originally proposed in [3] and reconsidered several times in the literature, see e.g. [5; 6; 7] and the references therein. The FIR model has length  $M = 5$  and is characterized by the coefficients

$$h = [-0.3 \quad -0.9 \quad 0.8 \quad -0.7 \quad 0.6]^T. \quad (110)$$

The input signal is the autoregressive process

$$x(t) = -0.2x(t-1) - 0.6x(t-2) + w(t), \quad (111)$$

where  $w(t)$  is a Gaussian white noise with unit variance.

In order to illustrate the effect of the transient term with respect to the amount of noise, Figure 2 reports, for different data lengths  $N$ , the values of  $\rho$ , see eq. (56), and  $\delta$ , see eq. (57) for different values of the signal-to-noise ratio (SNR).

To complete this analysis, a Monte Carlo simulation of 100 independent runs has been performed in the case of very short data,  $N = 25$ , with very small amount of noise, SNR = 60 dB. Table 1 reports the empirical means of the system parameter estimates obtained by means of the Algorithm 1 when the transient term is taken into account, as described in Section 5 (FIR1-FD) and when the transient term is not considered, as described in the Remarks 3 and 6 (FIR1-FD-NT). The number of the HOYW equations has been fixed to the minimal values  $q = 2M - 1 = 9$  and  $q = M = 5$ , respectively.

A second Monte Carlo of 100 independent runs has been performed by considering noisy input and output sequences of length  $N = 100$ , affected by additive white noises corresponding to a SNR of 20 dB on both input and output sides.



Table 1. True and estimated parameters with and without the transient term -  $N = 25$ , SNR = 60 dB.

	$h_0$	$h_1$	$h_2$	$h_3$	$h_4$
true	-0.3	-0.9	0.8	-0.7	0.6
FIR1 - FD	$-0.2998 \pm 0.6635 * 10^{-3}$	$-0.8999 \pm 0.5814 * 10^{-3}$	$0.8001 \pm 0.6782 * 10^{-3}$	$-0.7000 \pm 0.5469 * 10^{-3}$	$0.5999 \pm 0.7329 * 10^{-3}$
FIR1 - FD - NT	$-0.4594 \pm 0.0009$	$-1.1020 \pm 0.0012$	$0.5219 \pm 0.0016$	$-0.7924 \pm 0.0011$	$0.4451 \pm 0.0010$

Table 2. True and estimated parameters obtained with FIR1-FD, FIR2-FD, FIR1-TD, FIR2-TD and TLS-TD -  $N = 100$ , SNR = 20 dB.

	true	FIR1 - FD	FIR2 - FD	FIR1 - TD	FIR2 - TD	TLS - TD
$h_0$	-0.3	$-0.2983 \pm 0.0243$	$-0.3032 \pm 0.0254$	$-0.2990 \pm 0.0261$	$-0.3024 \pm 0.0271$	$-0.2990 \pm 0.0263$
$h_1$	-0.9	$-0.9039 \pm 0.0261$	$-0.9097 \pm 0.0695$	$-0.9022 \pm 0.0271$	$-0.9094 \pm 0.0917$	$-0.9050 \pm 0.0238$
$h_2$	0.8	$0.7970 \pm 0.0306$	$0.7906 \pm 0.0446$	$0.7970 \pm 0.0316$	$0.7953 \pm 0.0534$	$0.7985 \pm 0.0321$
$h_3$	-0.7	$-0.7040 \pm 0.0238$	$-0.7107 \pm 0.0472$	$-0.7031 \pm 0.0243$	$-0.7091 \pm 0.0537$	$-0.7046 \pm 0.0233$
$h_4$	0.6	$0.5975 \pm 0.0253$	$0.5945 \pm 0.0576$	$0.5969 \pm 0.0254$	$0.5978 \pm 0.0735$	$0.5993 \pm 0.0260$
$\sigma_o^*$	0.0207	$0.0206 \pm 0.0208$	$0.0155 \pm 0.0975$	$0.0234 \pm 0.0225$	$0.0138 \pm 0.1310$	$0.0194 \pm 0.0031$
$\sigma_i^*$	0.0113	$0.0093 \pm 0.0088$	$0.0858 \pm 0.0278$	$0.0089 \pm 0.0090$	$0.0835 \pm 0.0328$	$0.0106 \pm 0.0017$

Table 2 reports the empirical means of the system parameter estimates and of the noise variance estimates, together with the corresponding standard deviations, obtained with the algorithms proposed in Sections 5 and 6, denoted with FIR1-FD and FIR2-FD, respectively. The number of the HOYW equations has been fixed to  $q = 2M - 1 = 9$  for both algorithms. The table shows also the results obtained with the corresponding time domain algorithms, denoted with FIR1-TD and FIR2-TD. The FIR2-TD algorithm was originally described in [5]. For FIR1-TD and FIR2-TD the number of the HOYW equations has been fixed to  $q = M = 5$ . For comparison, the last column of the table reports also the estimates obtained with the classical (time-domain) total least-squares method [8; 12]. Of course, to obtain the TLS-TD solution, the noise variance ratio  $\sigma_o^*/\sigma_i^*$  has been considered as *a priori* known. The TLS estimate should therefore be seen as a lower (and not accessible) limit of the performance, as TLS is heavily exploiting the detailed information of known  $\sigma_o^*/\sigma_i^*$  [24]. It can be observed that the proposed identification methods yield similar, good results. Very similar results are also obtained by means of the corresponding time domain versions.

For a deeper comparison of the asymptotic performances of the proposed algorithms, a Monte Carlo simulation of 100 independent runs has been carried out with  $N = 500$ , by considering different values of the SNR. In every run, the SNRs on the input and output sides are equal. The normalized root mean square error

$$\text{NRMSE} = \frac{1}{\|h\|} \sqrt{\frac{1}{100} \sum_{i=1}^{100} \|\hat{h}^i - h\|^2} \quad (112)$$

has been used as performance index, where  $\hat{h}^i$  denotes the estimates of  $h$  obtained in the  $i$ -th trial of the Monte Carlo simulation. The results are shown in Figure 3. Note that for high values of the SNR, the curves tend all to be straight lines with slope  $-1$ . This means that for high SNR values, NRMSE is inversely proportional to SNR, and it holds

$$\text{NRMSE} \sim \frac{1}{\text{SNR}}. \quad (113)$$

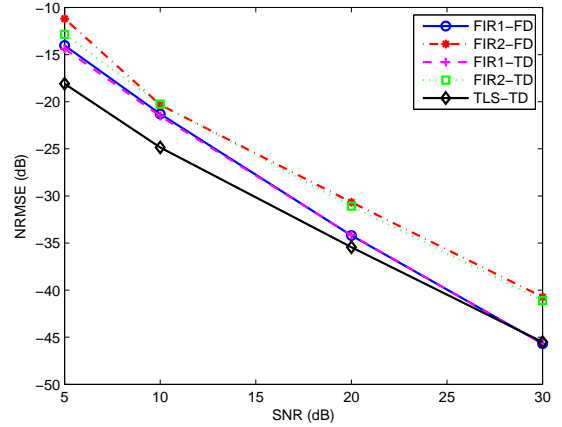


Fig. 3. NRMSE versus SNR: FIR1-FD (circle, solid), FIR2-FD (dashed-dotted), FIR1-TD (dashed), FIR2-TD (dotted), TLS-TD (diamond, solid).

It can be observed that the performances of the FIR1 algorithms are slightly better than those of the corresponding FIR2 algorithms.

Concluding, with reference to the case of  $N = 100$  and SNR = 20 dB, the Figure 4 reports the results of the model order estimate, obtained with the cost function  $J_n$  in (107), evaluated by means of the two proposed algorithms. It can be observed that the Algorithm 1 yields a nicer, monotonic, behavior of  $J_n$ .

*Example 2.* In this example a FIR model with length  $M = 25$ , used in [21], has been considered. The parameters are reported in the first column of Table 3. The input signal  $x(t)$  is a Gaussian white noise with variance  $\sigma_x = 1$ . A Monte Carlo simulation of 100 independent runs has been performed with very small amount of noise, SNR = 60 dB. The second column of Table 3 reports the empirical means of the system parameter estimates obtained by means of the Algorithm 1 when the transient term is taken into account (FIR1-FD) with a data sequence of length  $N = 100$ . The third column reports the results obtained when the transient term is not considered (FIR1-FD-NT).

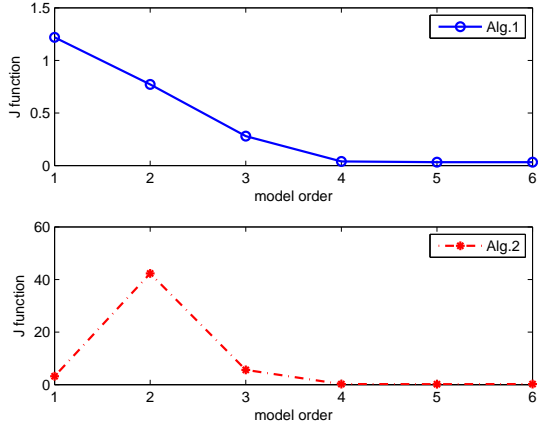


Fig. 4. Function  $J_n$  versus the model order  $n$ .  $N = 100$ , SNR= 20 dB.

Table 3. True and estimated parameters, SNR= 60dB.

	true	FIR1 – FD $N = 100$	FIR1 – FD – NT $N = 1000$
$h_0$	-0.0160	-0.0159 ± 0.0009	-0.0229 ± 0.1602 * 10 <sup>-3</sup>
$h_1$	0.0070	0.0071 ± 0.0012	0.0167 ± 0.2050 * 10 <sup>-3</sup>
$h_2$	0.0700	0.0701 ± 0.0012	0.0930 ± 0.2259 * 10 <sup>-3</sup>
$h_3$	0.1450	0.1449 ± 0.0010	0.1518 ± 0.2256 * 10 <sup>-3</sup>
$h_4$	0.1430	0.1428 ± 0.0011	0.1301 ± 0.2116 * 10 <sup>-3</sup>
$h_5$	-0.0130	-0.0129 ± 0.0011	-0.0311 ± 0.2000 * 10 <sup>-3</sup>
$h_6$	-0.2870	-0.2869 ± 0.0011	-0.2931 ± 0.2011 * 10 <sup>-3</sup>
$h_7$	-0.2800	-0.2799 ± 0.0011	-0.2936 ± 0.2152 * 10 <sup>-3</sup>
$h_8$	-0.2800	-0.2799 ± 0.0011	-0.2769 ± 0.2226 * 10 <sup>-3</sup>
$h_9$	0.4280	0.4279 ± 0.0011	0.4401 ± 0.2321 * 10 <sup>-3</sup>
$h_{10}$	0.1490	0.1490 ± 0.0011	0.1778 ± 0.2142 * 10 <sup>-3</sup>
$h_{11}$	2.4560	2.4560 ± 0.0011	2.4513 ± 0.2005 * 10 <sup>-3</sup>
$h_{12}$	2.8470	2.8469 ± 0.0009	2.8389 ± 0.1853 * 10 <sup>-3</sup>
$h_{13}$	2.4560	2.4559 ± 0.0010	2.4522 ± 0.2220 * 10 <sup>-3</sup>
$h_{14}$	1.4900	1.4899 ± 0.0010	1.4951 ± 0.2169 * 10 <sup>-3</sup>
$h_{15}$	0.4280	0.4280 ± 0.0012	0.4338 ± 0.2046 * 10 <sup>-3</sup>
$h_{16}$	-0.2800	-0.2798 ± 0.0011	-0.2748 ± 0.2375 * 10 <sup>-3</sup>
$h_{17}$	-0.4700	-0.4701 ± 0.0010	-0.4626 ± 0.2442 * 10 <sup>-3</sup>
$h_{18}$	-0.2870	-0.2872 ± 0.0010	-0.2727 ± 0.2200 * 10 <sup>-3</sup>
$h_{19}$	-0.0130	-0.0130 ± 0.0010	-0.0173 ± 0.2186 * 10 <sup>-3</sup>
$h_{20}$	0.1430	0.1429 ± 0.0010	0.1396 ± 0.2402 * 10 <sup>-3</sup>
$h_{21}$	0.1450	0.1451 ± 0.0010	0.1396 ± 0.2265 * 10 <sup>-3</sup>
$h_{22}$	0.0700	0.0699 ± 0.0009	0.0634 ± 0.2134 * 10 <sup>-3</sup>
$h_{23}$	0.0070	0.0070 ± 0.0010	-0.0024 ± 0.2262 * 10 <sup>-3</sup>
$h_{24}$	-0.0160	-0.0158 ± 0.0010	-0.0148 ± 0.1847 * 10 <sup>-3</sup>

In this case a longer data sequence with  $N = 1000$  has been considered, in order to better satisfy the asymptotic conditions recalled in the Remark 6. The number of the HOYW equations has been fixed to the minimal values  $q = 2M - 1$  and  $q = M$ , respectively.

This example points out an interesting result, that well explains the difference between the theoretical aspects described in this

paper and the practical approaches often used in frequency identification, see also Remark 6. In the presence of very low noise (SNR=60dB), and taking into account the transient effect, the proposed algorithm yields very good estimates of the parameters with only 100 samples (4 times the length of the filter). In the same SNR conditions, without taking into account this effect, even working with 1000 samples, the estimates of the parameters are less accurate, even if the reconstruction of the frequency spectrum (not reported here) is fairly good for practical applications.

*Example 3.* In order to compare the two proposed methods against other time domain methods, the following FIR model, with length  $M = 5$ , has been considered

$$h = [1.0000 \quad -0.3903 \quad 0.6240 \quad -0.1912 \quad 0.2401]^T. \quad (114)$$

The input signal  $x(t)$  is a Gaussian white noise with variance  $\sigma_x = 1$ . A Monte Carlo of 100 independent runs has been performed by considering noisy input and output sequences of length  $N = 100$ , affected by additive white noises corresponding to a SNR of 20 dB on both input and output sides.

Table 4 reports the empirical means of the system parameter estimates and of the noise variance estimates, together with the corresponding standard deviations, obtained with the FIR1-FD and FIR2-FD algorithms. For comparison, the last two columns of Table 4 report the results obtained by means of the time domain GIVE method (GIVE-TD) [23] and the time domain Instrumental Variable method (IV-TD) [28], respectively. For the IV method, the vector of instruments was taken as

$$z(t) = (u(t - M) \dots u(t - 2M + 1))^T, \quad (115)$$

leading to precisely  $M$  linear equations for determining the  $M$  unknown elements of  $h$ . For the GIVE method, the vector of generalized instruments was taken as

$$z(t) = (y(t) y(t - 1) u(t) \dots u(t - M - 1))^T, \quad (116)$$

leading to an overdetermined system of  $M + 4$  equations for determining the  $M + 2$  unknowns (the  $M$  elements of  $h$ , and the noise variances  $\sigma_i^*$  and  $\sigma_o^*$ ). Equal weighting was applied when solving this nonlinear least squares system of equations. It can be observed that the FIR1-FD and the GIVE methods yield similar, good results, while the performance of the FIR2-FD is slightly inferior. As expected, the IV method yields bad estimates for such a short data record.

The next numerical example illustrates the frequency domain features of the new identification methods, described in the Subsection 7.2.

*Example 4.* The same FIR model of the Example 3 has been considered

$$h = [1.0000 \quad -0.3903 \quad 0.6240 \quad -0.1912 \quad 0.2401]^T. \quad (117)$$

The input signal  $x(t)$  is a Gaussian white noise with variance  $\sigma_x = 1$ . In this example the input measurement noise is not present, i.e.  $n_i(t) = 0$ , and the output signal is affected by a pink noise. Pink noise is frequently used in music signal processing and is characterized by a power spectrum that falls in frequency like  $1/f$ . The pink noise has been generated by using the following third-order ARMA model, suggested in [17] at pag. 736

$$n_o(t) = g_0 \frac{B(z^{-1})}{A(z^{-1})} e(t), \quad (118)$$

where  $e(t)$  is a white noise with variance  $\sigma_e$ ,  $g_0 = 0.57534$  and

Table 4. True and estimated parameters obtained with FIR1-FD, FIR2-FD, IV-TD and GIVE-TD -  $N = 100$ , SNR = 20 dB.

	true	FIR1 - FD	FIR2 - FD	GIVE - TD	IV - TD
$h_0$	1.0000	1.0007 ± 0.0139	0.9877 ± 0.0649	1.0062 ± 0.0181	0.8065 ± 4.3999
$h_1$	-0.3903	-0.3914 ± 0.0183	-0.3826 ± 0.0261	-0.3943 ± 0.0186	-0.1887 ± 6.2456
$h_2$	0.6240	0.6247 ± 0.0162	0.6214 ± 0.0370	0.6226 ± 0.0151	0.4597 ± 5.9754
$h_3$	-0.1912	-0.1931 ± 0.0180	-0.1894 ± 0.0226	-0.1913 ± 0.0185	-0.0900 ± 4.2247
$h_4$	0.2401	0.2412 ± 0.0183	0.2319 ± 0.0336	0.2449 ± 0.0191	0.1430 ± 2.7857
$\sigma_o^*$	0.0125	0.0124 ± 0.0106	0.0271 ± 0.0720	0.0112 ± 0.0120	—
$\sigma_i^*$	0.0075	0.0060 ± 0.0065	0.1364 ± 0.0391	0.0116 ± 0.0094	—

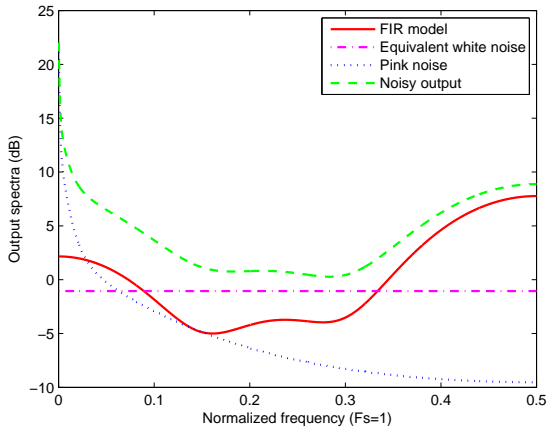


Fig. 5. FIR model (solid), pink noise (dotted), equivalent white noise (dash-dotted) and noisy signal (dashed)

$$B(z^{-1}) = (1 - 0.98444 z^{-1})(1 - 0.83392 z^{-1}) \times (1 - 0.07568 z^{-1}) \quad (119)$$

$$A(z^{-1}) = (1 - 0.99574 z^{-1})(1 - 0.94791 z^{-1}) \times (1 - 0.53568 z^{-1}). \quad (120)$$

The resulting power spectra of the signals  $d(t)$  and  $n_o(t)$  are

$$S_d(\omega_k) = |H(e^{-j\omega_k})|^2 \sigma_x = |H(e^{-j\omega_k})|^2 \quad (121)$$

$$S_{n_o}(\omega_k) = g_0^2 \frac{|B(e^{-j\omega_k})|^2}{|A(e^{-j\omega_k})|^2} \sigma_e. \quad (122)$$

By construction, asymptotically, when  $N \rightarrow \infty$ , the variance  $\sigma_e$  coincides with the variance of the output noise  $n_o(t)$ , i.e.  $\sigma_e = \sigma_o^*$ . For this reason, the data length in this example has been fixed to  $N = 5000$ .

A Monte Carlo of 100 independent runs has been performed by considering noisy output sequences, affected by additive pink noise, with variance  $\sigma_o^* = 0.7833$ , corresponding to a ratio

$$10 \log_{10} \frac{S_d(\omega_k)}{S_{n_o}(\omega_k)} = 10 \log_{10} \frac{|H(e^{-j\omega_k})|^2}{\sigma_o^*} \quad (123)$$

of about 3 dB for  $\omega_k = 0$ .

Figure 5 shows the spectrum of the FIR system (solid line) and the spectrum of the additive pink noise (dotted line) together with the resulting noisy output spectrum (dashed line). The dash-dotted line reports the spectrum of the equivalent white noise with variance  $\sigma_o^*$ .

In many real situations some additional information about the system is available. In this case, for example, one could be

Table 5. True and estimated parameters in the presence of output pink noise

	true	FIR1 - FD [0.15 - 0.5]	FIR1 - FD [0 - 0.5]
$h_0$	1.0000	1.0061 ± 0.0106	1.0912 ± 0.1172
$h_1$	-0.3903	-0.3856 ± 0.0133	-0.4333 ± 0.0607
$h_2$	0.6240	0.6315 ± 0.0157	0.6840 ± 0.0779
$h_3$	-0.1912	-0.1860 ± 0.0130	-0.2132 ± 0.0345
$h_4$	0.2401	0.2427 ± 0.0095	0.2601 ± 0.0286
$\sigma_o^*$	0.7833	0.1096 ± 0.0038	0.6138 ± 0.0885
$\sigma_i^*$	0.0000	0.0018 ± 0.0022	0.0726 ± 0.1378

aware that the additive noise is of pink type. Taking account of this information, the FIR model has been identified by using the FIR1-FD algorithm within the frequency window  $F = [f_i, f_f]$ , with  $f_i = 0.15$  and  $f_f = 0.5$ . In this way, the effect of the pink noise, acting at low frequencies, has been filtered out.

The results of the simulation are reported in the first column of Table 5. For comparison, the second column of Table 5 reports the estimates obtained by the same FIR1-FD algorithm when the whole frequency window  $F = [0, 0.5]$  is used. The advantageous effects of filtering are evident. In fact the method yields accurate estimates of the system parameters. It can be observed that the results using all frequencies are definitely worse.

## 9. CONCLUSIONS

In this paper a novel frequency domain approach has been proposed for the identification of FIR models affected by additive white noises. In particular, two different frequency domain algorithms have been proposed and their estimation properties have been tested and compared by means of Monte Carlo simulations. The numerical results have confirmed the good performances of the proposed methods. The benefits of filtering the data in the frequency domain have been illustrated by means of a numerical example.

## Appendix A. PROOFS OF THE THEOREMS IN SECTION 4

*Proof of Theorem 1.* According to partition (60), we have

$$R - \tilde{R} = \begin{bmatrix} r_{11} - \sigma_o & R_{12} \\ R_{21} & R_{22} - \sigma_i I_M \end{bmatrix}, \quad (A.1)$$

with  $r_{11} - \sigma_o > 0$  and  $R_{22} - \sigma_i I_M > 0$ . The condition  $R - \tilde{R} \geq 0$  is equivalent to the diagonal expression, e.g. [28], pag. 512

$$\begin{bmatrix} r_{11} - \sigma_o & 0 \\ 0 & R_{22} - \sigma_i I_M - R_{21} (r_{11} - \sigma_o)^{-1} R_{12} \end{bmatrix} \geq 0 \quad (\text{A.2})$$

or, equivalently

$$\begin{bmatrix} r_{11} - \sigma_o - R_{12} (R_{22} - \sigma_i I_M)^{-1} R_{21} & 0 \\ 0 & R_{22} - \sigma_i I_M \end{bmatrix} \geq 0. \quad (\text{A.3})$$

The condition (A.2) implies that

$$\sigma_i \leq \lambda_{\min} \left( R_{22} - R_{21} (r_{11} - \sigma_o)^{-1} R_{12} \right). \quad (\text{A.4})$$

Since

$$\begin{aligned} \min_{\sigma_o} \lambda_{\min} \left( R_{22} - R_{21} (r_{11} - \sigma_o)^{-1} R_{12} \right) \\ = \lambda_{\min} \left( R_{22} - R_{21} (r_{11})^{-1} R_{12} \right), \end{aligned} \quad (\text{A.5})$$

we have

$$\sigma_i \leq \sigma_i^{\max} = \lambda_{\min} \left( R_{22} - \frac{R_{21} R_{12}}{r_{11}} \right). \quad (\text{A.6})$$

Analogously, the condition (A.3) implies that

$$\sigma_o \leq \lambda_{\min} \left( r_{11} - R_{12} (R_{22} - \sigma_i I_M)^{-1} R_{21} \right). \quad (\text{A.7})$$

Since the expression (A.7) is scalar, we have

$$\begin{aligned} \min_{\sigma_i} \left( r_{11} - R_{12} (R_{22} - \sigma_i I_M)^{-1} R_{21} \right) \\ = r_{11} - R_{12} R_{22}^{-1} R_{21} \end{aligned} \quad (\text{A.8})$$

so that

$$\sigma_o \leq \sigma_o^{\max} = r_{11} - R_{12} R_{22}^{-1} R_{21} = \frac{\det(R)}{\det(R_{22})}. \quad (\text{A.9})$$

*Proof of Theorem 2.* In general, from (A.2), for every value  $\sigma_o \in [0, \sigma_o^{\max}]$ , the corresponding value of  $\sigma_i$  that satisfies the conditions  $R - \tilde{R} \geq 0$  is obtained by

$$\sigma_i = \lambda_{\min} \left( R_{22} - \frac{R_{21} R_{12}}{(r_{11} - \sigma_o)} \right). \quad (\text{A.10})$$

Analogously, from (A.3), for every value  $\sigma_i \in [0, \sigma_i^{\max}]$ , the corresponding value of  $\sigma_o$  that satisfies the conditions  $R - \tilde{R} \geq 0$  is obtained by

$$\sigma_o = r_{11} - R_{12} (R_{22} - \sigma_i I_M)^{-1} R_{21}. \quad (\text{A.11})$$

It can be observed that when  $\sigma_i$  increases from 0 to  $\sigma_i^{\max}$ , the corresponding value of  $\sigma_o$ , determined by (A.11), decreases from  $\sigma_o^{\max}$  to 0. Thus, the points  $P = (\sigma_i, \sigma_o)$  of  $\mathcal{S}(R)$  describe a continuous curve in the first quadrant of  $\mathcal{R}^2$ .

*Proof of Theorem 3.* Consider an arbitrary point  $\bar{P} = (\bar{\sigma}_i, \bar{\sigma}_o)$  of  $\mathcal{S}(R)$  that satisfies the equation (A.11)

$$\bar{\sigma}_o = r_{11} - R_{12} (R_{22} - \bar{\sigma}_i I_M)^{-1} R_{21}. \quad (\text{A.12})$$

Let  $x$  be an infinitesimal perturbation on  $\bar{\sigma}_i$ . Defining  $\bar{R}_{22} = R_{22} - \bar{\sigma}_i I_M$ , the right-hand side in (A.12) results

$$f(x) = r_{11} - R_{12} (R_{22} - (\bar{\sigma}_i + x) I_M)^{-1} R_{21} \quad (\text{A.13})$$

$$= r_{11} - R_{12} (\bar{R}_{22} - x I_M)^{-1} R_{21} \quad (\text{A.14})$$

Note that  $f(0)$  represents the point  $\bar{P}$  on the curve  $\mathcal{S}(R)$ , in fact

$$f(0) = r_{11} - R_{12} \bar{R}_{22}^{-1} R_{21} = \bar{\sigma}_o. \quad (\text{A.15})$$

For simplicity, assume that the symmetric, positive definite matrix  $\bar{R}_{22}$  has all distinct eigenvalues  $\lambda_i > 0$ , with associated eigenvectors  $v_i$  ( $i = 1, \dots, M$ ). The resolvent of  $\bar{R}_{22}$ , see e.g. [15], can be written

$$R(x) = (x I_M - \bar{R}_{22})^{-1} = \sum_{i=1}^M \frac{v_i v_i^T}{x - \lambda_i}. \quad (\text{A.16})$$

Substituting (A.16) in (A.14), we have

$$f(x) = r_{11} - R_{12} \sum_{i=1}^M \frac{v_i v_i^T}{\lambda_i - x} R_{21}. \quad (\text{A.17})$$

The first and second derivatives of  $f(x)$  in (A.17) are

$$f'(x) = -R_{12} \sum_{i=1}^M \frac{v_i v_i^T}{(\lambda_i - x)^2} R_{21} \quad (\text{A.18})$$

$$f''(x) = -R_{12} \sum_{i=1}^M \frac{2 v_i v_i^T}{(\lambda_i - x)^3} R_{21}. \quad (\text{A.19})$$

Since  $\lambda_i > 0$  ( $i = \dots, M$ ), it results in

$$f'(0) = -R_{12} \sum_{i=1}^M \frac{v_i v_i^T}{\lambda_i^2} R_{21} < 0 \quad (\text{A.20})$$

$$f''(0) = -R_{12} \sum_{i=1}^M \frac{2 v_i v_i^T}{\lambda_i^3} R_{21} < 0. \quad (\text{A.21})$$

The condition (A.21) holds for all values  $\bar{\sigma}_i \in [0, \sigma_i^{\max}]$ . It means that the concavity of  $\mathcal{S}(R)$  faces the origin, since the tangent line in every point on  $\mathcal{S}(R)$  lies always over it.

*Proof of Theorem 4.* Since both  $\xi = (\xi_1, \xi_2)$  and  $P = (\sigma_i, \sigma_o)$  belong to  $r$  it follows that  $\xi = \lambda P$ . Since the entries of  $P$  must satisfy the condition  $R - \tilde{R}(P) \geq 0$  it results

$$R - \frac{1}{\lambda} \tilde{R}_\xi \geq 0, \quad (\text{A.22})$$

where  $\tilde{R}_\xi$  is defined in (64). Since  $R > 0$ , condition (A.22) is equivalent to

$$I_{M+1} - \frac{1}{\lambda} R^{-1} \tilde{R}_\xi \geq 0. \quad (\text{A.23})$$

The scalar  $\lambda$  that solves (A.23) is given by

$$\lambda_M = \lambda_{\max} (R^{-1} \tilde{R}_\xi). \quad (\text{A.24})$$

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